Switched Linear Multi-Robot Navigation Using Hierarchical Model Predictive Control

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Abstract

Multi-robot navigation control in the absence of reference trajectory is rather challenging as it is expected to ensure stability and feasibility while still offer fast computation on control decisions. The intrinsic high complexity of switched linear dynamical robots makes the problem even more challenging. In this paper, we propose a novel HMPC based method to address the navigation problem of multiple robots with switched linear dynamics. We develop a new technique to compute the reachable sets of switched linear systems and use them to enable the parallel computation of control parameters. We present theoretical results on stability, feasibility and complexity of the proposed approach, and demonstrate its empirical advance in performance against other approaches.

1 Introduction

A switched linear system is a special type of hybrid systems. It consists of a collection of modes described by linear dynamics (differential/difference equations), together with a switching rule specifying how to switch between the modes. It provides an expressive model used in designing robots which embrace complex behaviors [Faust et al., 2016; Bogomolov et al., 2014; Lahijanian et al., 2014]. For example, a robot equipped with many gears which deliver different torques and speeds can be directly modeled by a switched linear system.

The multi-robot navigation problem has been attracting much attention for being not only academically challenging, but also of practical importance. The navigation is to drive a group of robots from their initial positions to goal positions without any reference trajectory. A successful navigation should provide three guarantees: converging to the goal positions finally (stability), avoiding collision all the time (feasibility), fast computing (efficiency).

There have been a number of works treating the navigation problems as path planning problems, where heuristic-search based methods are the most popular and well-developed solutions [Wagner and Choset, 2011; Karaman and Frazzoli, 2011; Janovsky et al., 2014]. For robots with discrete state space such as graph, A* based algorithms can quickly find the optimal path while ensuring the stability, and thus are well studied [Koenig and Likhachev, 2002; Wagner and Choset, 2011]. Before adopting it to robots with continuous states, the continuous state space must be discretized in advance. Those methods that deal with continuous state space directly receive much attention in recent years. Optimal reciprocal collision avoidance (ORCA) approach [van den Berg et al., 2011] is proposed to address the collision avoidance problem of robots. It is then combined with the RRT* algorithm [Karaman and Frazzoli, 2011], an extension of RRT (rapidly exploring random tree), for robot navigation in a continuous state space [Janovsky et al., 2014]. However neither of them ensure theoretical stability, therefore may easily lead robots to a saturation where robots stick at one point as a result of infinite loops or deadlock [Janovsky et al., 2014]. Note that, to ease treatment, all the above methods assume that once the specified positions are given, all robots can easily compute the corresponding inputs and arrive the positions accurately, and thus do not take the concrete dynamics of robots into consideration.

Unfortunately, as is pointed in [Pecora et al., 2012], for robots with complex behaviors, treating the navigation problem as two separated steps: path panning and control inputs computation may cause severe collision issues. That is, due to the absence of robot behavior in path planning, even though the planned path is theoretically safe, in practice it might lead to collisions as the target positions in the given trajectory may be beyond the robots’ ability. Therefore, for switched linear robots, due to their intrinsic complexity, the strategy of separation does not fit for handling the navigation problems.

Different from path planning approaches which only consider the trajectory, the switched linear robot navigation control requires to compute control inputs of all robots with consideration of robot dynamics. Model Predictive Control (MPC) is the most popular method whose basic idea is to first compute an input sequence of the next several steps using certain path finding strategy, and then choose the sequence head as the current input. MPCs can be mainly divided into three categories: centralized MPC (CMPC), distributed MPC (DMPC) and hierarchical MPC (HMPC). CMPC provides theoretical guarantee on feasibility and stability, but suffers from a high computation complexity. DMPCs can hardly ensure the stability under (non-convex) collision avoidance specification. Recently, HMPCs are proposed which balance the
merits of both CMPC and DMPC schemes. In HMPC framework, a central controller determines the next state of every robot while for each robot, there is a distributed controller computing its control parameter driving it to the given state. Among them, the approach proposed in [Cirillo et al., 2014] cannot ensure the dynamic feasibility generated by the central controller and the method proposed in [Huang et al., 2016] replaces constraints of dynamics with reachable sets of robots so that the goal states can be efficiently produced by the central controller, ensuring both stability and feasibility for simple linear dynamical robots.

In this paper, starting from the reachable set based HMPC, we aim to address the navigation problem of robots whose behaviors are described by switched linear systems in continuous space. The key challenge in such a HMPC is how to compute the exact reachable set of robots in a very short time: the accuracy of the reachable sets assures the equivalence between the transformed optimization problem and the original one; if the overhead incurred by the computation of reachable sets is more than the time saving made by parallel computation, it would render HMPC to be less useful. The reachable set computation of general switched systems is a well-known undecidable problem which requires heavy computation efforts [Alur et al., 1995; Henzinger et al., 1995]. We give a novel method to compute the reachable set function by slightly restricting the multi-robot system with two reasonable assumptions. The reachable set function is computed in advance off-line, and the concrete reachable set is directly on-line derived by substituting the current state. Our main contributions are listed as follows:

- We propose a novel HMPC based method to address the navigation problem of switched linear multi-robot using our newly developed technique to compute the reachable set function of switched linear systems.
- We theoretically ensure the feasibility and stability of the proposed method and discuss its complexity;
- We demonstrate the performance of the new HMPC based method in several navigation scenarios and show its advantages empirically by varied comparison.

2 Problem Formulation

Consider a switched linear dynamical multi-robot system \( S \) containing \( N \) robots on a plane. Assuming the sampling interval of the \( i \)-th robot is \( T_r \), robots will synchronize with each other at the end of every collaboration cycle, which is the least common multiple of robots’ sampling intervals.

Before we formally describe the systems and problem, we first introduce two main assumptions throughout this paper.

**Assumption 1.** Each robot has independent dynamics and inputs along the \( x \)-axis and \( y \)-axis.

**Assumption 2.** Each robot stay stationary at a collaboration instant.

These two assumptions are not strict to multi-robot navigation control. Assumption 1 is a general setting in a lot of works [Wang et al., 2007]. For Assumption 2, notably in current works of multi-robot navigation control, in particular heuristic-search methods, forcing robots to stop is a common choice when confronted with conflicting situations [Wei et al., 2014].

Now, we model such a multi-robot system. For the \( i \)-th robot, the collaboration cycle is \( K_i \) times its local control cycle. A state of the \( i \)-th robot is denoted as \( q_i = [x_i, \dot{x}_i, y_i, \dot{y}_i]^T \), where \( x_i, \dot{x}_i, y_i, \dot{y}_i \) denote the position and velocity along the \( x \)-axis and the \( y \)-axis, respectively. Let \( q_{ix} = [x_i, \dot{x}_i]^T \) and \( q_{iy} = [y_i, \dot{y}_i]^T \) be the states along two axes. Since the dynamics of each robot along two axes are independent, we can model the dynamic along each axis separately as a switched linear system. Let \( M_{ix} \) and \( M_{iy} \) be the number of permissible linear dynamical modes along \( x \)-axis and \( y \)-axis. For the \( x \)-axis, the dynamic is modeled as the linear discrete-time time-varying state equality below:

\[
q_{ix}(k, k+1) = A_{ix} q_{ix}(k, k) + B_{ix}(m_{ix}(k, k_i)) u_{ix}(k, k_i),
\]

where \( k \) denotes the \( k \)-th collaboration instant, \( k_i \in \{0, 1, ..., K_i - 1\} \) represents the \( k_i \)-th local sampling instant of the \( i \)-th robot, the pair \((m_{ix}(k, k_i), u_{ix}(k, k_i))\) is referred as the hybrid control along the \( x \)-axis, where:

**Switching Control** \( m_{ix}(k, k_i) \in M_{ix} = \{1, ..., M_{ix}\} \) determines the dynamic mode;

**Continuous Control** \( u_{ix}(k, k_i) \in U_{ix} = [-1, 1] \) determines the continuous evolution.

\( A_{ix} \) is the \( 2 \times 2 \) coefficient matrix of state \( q_{ix} \) while \( B_{ix} \) is the \( 2 \times 1 \) coefficient matrix of \( u_{ix} \) determined by \( m_{ix}(k, k_i) \). Equation (1b) defines the beginning state of one collaboration cycle as the ending state of the last collaboration cycle. Intuitively, Equation (1) indicates that the \( i \)-th robot can switch to one of the permissible dynamic modes along the \( x \)-axis at each sampling instant, then pick an appropriate input under the mode. Following the dynamic model along the \( x \)-axis, we model the one along the \( y \)-axis in the same way:

\[
q_{iy}(k, k+1) = A_{iy} q_{iy}(k, k) + B_{iy}(m_{iy}(k, k_i)) u_{iy}(k, k_i),
\]

where \( A_i = A_{ix} \oplus A_{iy}, B_i(m_{ix}(k, k_i)) = B_{ix}(m_{ix}(k, k_i)) \oplus B_{iy}(m_{iy}(k, k_i)) \), and the direct sum operation \( \oplus \) for two matrices \( A \) and \( B \) is defined as:

\[
A \oplus B \triangleq \begin{bmatrix} A & 0 \\ 0 & B \end{bmatrix}.
\]

The constraint of switching control is:

\[
m_{i}(k, k_i) \in M_i \triangleq M_{ix} \times M_{iy},
\]

which means that the \( i \)-th robot has \( M_{ix} \cdot M_{iy} \) dynamic modes. The switching control sequence of the \( i \)-th robot in the \( k \)-th collaboration cycle is denoted by \( \tilde{m}_i(k) \triangleq m_i(k, 1), ..., m_i(k, K_i - 1) \). The constraint of continuous control is:

\[
u_{i}(k, k_i) \in U_i \triangleq U_{ix} \times U_{iy} = [-1, 1].
\]
where \( U_i = [U_{i,x}, U_{i,y}]^T \). The continuous control sequence of the \( i \)-th robot in the \( K \)-th collaboration cycle is denoted by \( \tilde{u}_i(k) \triangleq u_i(k), u_i(k, 1), \ldots, u_i(k, K_t-1) \). We refer to the pair \((m_i(k, k_i), u_i(k, k_i))\) as the hybrid control of the \( i \)-th robot.

For a multi-robot system \( S \), let \( q(k) \triangleq [q_1(k), \ldots, q_N(k)] \) denote the global state at the \( k \)-th collaboration instant, \( \tilde{r}_i(k) \triangleq \tilde{r}_1(k), \ldots, \tilde{r}_N(k) \) and \( \tilde{u}_i(k) \triangleq \tilde{u}_1(k), \ldots, \tilde{u}_N(k) \) denote the global switching and continuous control sequence in the \( k \)-th collaboration cycle respectively.

Assumption 2 is described as collaboration specification:

\[
\dot{x}_i(k) = \tilde{y}_i(k) = 0, \quad k \geq 0, \quad (6)
\]

We define the collision avoidance specification requiring that the (infinity norm) distance between any two robots must not be less than a given safety distance \( d_{\text{safe}} \):

\[
h_i(q) \leq 0, \quad k \geq 0, \quad (7)
\]

where

\[
h_i(q) = [h_{i,j}(q_i, q_j)]_{l_i,j=1}^{N_i}
\]

\[
h_{i,j}(q_i, q_j) = \begin{cases} d_{\text{safe}} - \|q_{i,\text{pos}} - q_{j,\text{pos}}\| & , i \neq j, \\ 0, & i = j. \end{cases}
\]

The infinite norm of a vector \( x = [x_1, \ldots, x_n]^T \) is defined as \( \|x\|_{\infty} \triangleq \max \{|x_1|, \ldots, |x_n|\} \).

Following [Huang et al., 2016], we define two core concepts for MPC, namely feasibility and stability.

**Definition 1.** (Feasibility) A MPC controller is feasible if for any feasible initial state, the actual state \( \{q(t), t \geq 0\} \) computed by the controller at every collaboration instant satisfies the collision avoidance specification \( h_i(q(t)) \leq 0 \).

**Definition 2.** (Stability) A MPC scheme is stable if starting from any feasible initial state, the state sequence \( \{q(t)\}_{t=0}^{\infty} \) computed by the MPC controller converges to the goal state.

Subsequently we formulate the navigation problem:

**Problem 1.** Given a multi-robot system \( S \), where

- the \( i \)-th robot has the kinematic model described as in (3a) and (3b) with switching control constraint (4) and continuous control constraint (5);
- a stationary initial state \( q(0) = [q_1(0), \ldots, q_N(0)]^T \) of \( S \), where the initial velocity of each robot is zero;
- a stationary goal state \( q^* = [q_1^*, \ldots, q_N^*]^T \) of \( S \), where the goal velocity of each robot is zero;
- the collaboration specification and collision avoidance specification are described as in (6) and (7) respectively.

Determine a control strategy to generate the hybrid control sequence \( \{(\tilde{m}_i(k), \tilde{u}_i(k))\}_{k=0}^{\infty} \) for the \( i \)-th robot, \( i=1, \ldots, N \), satisfying feasibility and stability.

**Remark 1.** In this work, we consider the obstacle-free navigation scenario. Note that for each robot, all other robots are treated as moving obstacles, and the collision avoidance is described by coordination constraints. With trivial extension, stationary obstacles can be treated similarly. Therefore, this setup does not lose the generality and practicality.

### 3 HMPC Framework

In this section, we briefly introduce the basic idea of the HMPC control framework on switched linear multi-robot navigation. At a collaboration instant \( t \), the HMPC scheme consists of two successive steps:

**Compute the control goals:** The central controller collects the current state \( q(t) \) and minimizes the state cost in a finite horizon \( H \):

\[
J^*_t(q(t)) \triangleq \begin{array}{ll}
\min_{q((t+1), t)]} \sum_{k=0}^{H-1} l_q(q(k|t)) + l_u(H|q(t)) \\
\text{s.t.} \quad q(k+1|t) \in R_i(q(k|t)), \quad k \geq 0, \quad i = 1, \ldots, N,
\end{array}
\]

where the notation \( (\cdot)|k(t) \) denotes the predictive value at the \((r+k)-th\) collaboration instant computed at time \( t \), \( R_i(q(k|t)) \) is the state set which the \( i \)-th robot can reach at the next collaboration instant from the state \( q_i(k|t) \), \( l_H \) and \( l_q \) are user-defined terminal cost and terminal constraint set to ensure stability. \( l_q \) and \( l_u \) denote the state cost and continuous control cost respectively, which are designed to be positive definite:

\[
l_q(q) = \begin{cases} 0, & q = q^*, \\
> 0, & q \neq q^*. \end{cases}, \quad \text{and} \quad l_u(u) = \begin{cases} 0, & u = 0, \\
> 0, & u \neq 0. \end{cases}
\]

Let \( q^*(1|t), \ldots, q^*(H|t) \) denote the optimal solution. The first sample \( q^*(1|t) \) will be used as the desired states \( q(t+1) \) at the instant \( t+1 \), that is \( q(t+1) = q^*(1|t) \). For the vector \( q(t+1) = [q_1(t+1), \ldots, q_N(t+1)]^T \), its \( i \)-th element \( q_i(t+1) \) specifies the control goal of the \( i \)-th robot at the collaboration instant \( t+1 \).

**Compute the hybrid controls:** The \( i \)-th robot receives the control goal \( q_i(t+1) \) and then derives the explicit control:

\[
J^*_t(q_i(t), q_i(t+1)) \triangleq \begin{array}{l}
\min_{m_i(t), u_i(t)} l_u(u_i(t)) \\
\text{s.t.} \quad q_i(t, k_i+1) = A_i q_i(t, k_i) + B_i (m_i(t, k_i)) u_i(t, k_i), \\
0 \leq k_i \leq K_t-1, \\
q_i(t + 1) = q_i(t, K_t), \\
m_i(k, k_i) \in M_i, \quad u_i(k, k_i) \in U_i.
\end{array}
\]

Note that this optimization problem is non-convex. It can be convert to mixed integer programming and solved by optimization solvers according to [Richards and How, 2005]. The optimal solution \( (\tilde{m}_i^*(t), \tilde{u}_i^*(t)) \) is the actual hybrid control sequence for the \( i \)-th robot in the next collaboration cycle.

This procedure will be repeated at the next collaboration instant \( t + 1 \) based on new measurements of the state \( q(t+1) \) until \( J^*_t(q(t)) \) meets a certain convergence criteria.

Observing HMPC framework, the key lies on how to efficiently compute the reachable set for switched linear systems.

### 4 Computation of Reachable Set Function

In this section, We propose a novel method for computing the reachable set function \( R_i(q_i(t)) \) for a switched linear system.

Recall the formal definition of a reachable set function.

**Definition 3.** The reachable set function \( R_i(q_i(t)) \) of the \( i \)-th robot is defined as the set comprising all states that the \( i \)-th
robot can reach in a collaboration cycle from the state \(q_i(t)\). In particular, \(RP_{i,x}(q_i(t))\) denotes the reachable position set function, which consists all the positions in \(R_i(q_i(t))\).

Consider the switching control sequence \(\dot{m}_i(t)\) in the \(i\)-th collaboration cycle. Since \(m_i(t, k_i)\) has \(M_{i,x} \times M_{i,y}\) choices at any \(k_i\)-th local sampling instant, \(\dot{m}_i(t)\) can have \((M_{i,x} \times M_{i,y})^{K_i}\) cases. And the reachable set under a certain switching control sequence is a polytope [Gritzmann and Sturmfels, 1993]. Hence a naïve way to compute \(R_i(q_i(t))\) is to directly compute the union of the \((M_{i,x} \times M_{i,y})^{K_i}\) convex polytopes. However, this approach faces a serious problem: if the representation of reachable set function includes the intermediate variables, its computation becomes time consuming and the optimization (9) solved in central controller degenerates to a CMPMC. It indicates two key requirements of reachable set function.

- **Requirement 1:** The computation of reachable set function should be efficient by reachable set function;

- **Requirement 2:** The representation of reachable set function should hide the intermediate variables between two collaboration instants.

In the following, we introduce our approach for computing the reachable set function \(R_i(q_i(t))\) under Assumption 1 and Assumption 2. Since the specification (6) demands \(\dot{x}_i(t+1) = y_i(t+1) = 0\), if we obtain the reachable position set \(RP_{i,x}(q_i(t)), R_i(q_i(t))\) can be easily computed as \(R_i(q_i(t)) = \{x, \dot{x}, y, \dot{y} \}^T = \{x, \dot{x}, y, \dot{y} \} \in RP_i(q_i(t)) \land (\dot{x}_i = y_i = 0)\). Hence the key is to compute \(RP_{i,x}(q_i(t))\).

Since the dynamic along the \(x\)-axis and \(y\)-axis is independent, we separately consider the dynamics along two axes. Let \(RP_{i,x}(q_i(t))\) and \(RP_{i,y}(q_i(t))\) denote the reachable position set along \(x\)-axis and \(y\)-axis, respectively. For the dynamic along the \(x\)-axis, we have the following conclusion.

**Lemma 1.** The reachable position set \(RP_{i,x}(q_i(t))\) along the \(x\)-axis is a closed interval.

**Proof.** For a switching control sequence \(\dot{m}_i(t) = (m_{i,x}(t, k_i))_{k_i=0}^{K_i-1}\) along with \(x\)-axis, let \(RP_{i,x}(q_i(t), m_{i,x}(t))\) be the reachable position set along the \(x\)-axis with \(m_{i,x}(t)\). Since \(RP_{i,x}(q_i(t))\) is a convex polytope [Gritzmann and Sturmfels, 1993] and is 1-dimensional, \(RP_{i,x}(q_i(t), m_{i,x}(t))\) is a closed interval. Furthermore, recall that

\[
\begin{align*}
q_{i,x}(t+1) &= A_{i,x} q_{i,x}(t, K_i - 1) + \sum_{p=0}^{K_i-1} (A_{i,x})^{K_i-p-1} B_{i,x}(m_{i,x}(t, p)) u_{i,x}(t, p), \\
&= A_{i,x} q_{i,x}(t, K_i - 2) + \sum_{p=0}^{K_i-1} (A_{i,x})^{K_i-p-1} B_{i,x}(m_{i,x}(t, K_i - 2)) u_{i,x}(t, K_i - 2) + \sum_{p=0}^{K_i-1} (A_{i,x})^{K_i-p-1} B_{i,x}(m_{i,x}(t, K_i - 1)) u_{i,x}(t, K_i - 1) + \cdots \tag{\text{A}_i(x)}
\end{align*}
\]

Obviously, \(\{m_{i,x}(t, k_i), 0\}_{k_i=0}^{K_i-1}\) is a feasible hybrid input sequence to make \(\dot{x}_i(t+1) = y_i(t+1) = 0\) for any switching control sequence \(\dot{m}_i(t)\). In this case, \(q_{i,x}(t+1) = (A_{i,x})^{K_i} q_{i,x}(t, K_i)\) and \(R_{i,x}(q_i(t), \dot{m}_i(t))\) is a closed interval. Then Lemma 1 can be proved by the property of intervals.

When \(q_{i,x}(t)\) is the origin, following Lemma 1, let \(RP_{i,x}(0) = \bigcap_{m_{i,x}(t) \in M_{i,x}} RP_{i,x}(q_i(t), \dot{m}_i(t))\). Then \(R_{i,x}(q_i(t))\) can be directly computed along the \(x\)-axis, where \(m_x(t)\) and \(max_x(t)\) denote the reachable position set along the \(x\)-axis, according to Assumption 2, we have

\[
\begin{align*}
RP_{i,x}(0) &= \{x : x = \sum_{k=0}^{K_i-1} (A_{i,x})^{K_i-k-1} B_{i,x}(m_{i,x}(t, p)) u_{i,x}(t, p), \\
&\quad u_{i,x}(t, p) \in U_i, m_{i,x}(t, p) \in M_{i,x}, p = 0, \ldots, K_i - 1\}
\end{align*}
\]

It immediately conducts the following corollary on the reachable position set from the above equation.

\[
RP_{i,x}(q_i(t)) = \{y : (x - (A_{i,x})^{K_i} q_{i,x}(t)) \in RP_{i,x}(0) \times \{0\} \times \{0\}\}
\]

Similarly, we can obtain the same conclusion on the dynamic along the \(y\)-axis. Let \(RP_{i,y}(0) = \{q_{i,y}(t) = [\min y_i, \max y_i]\}. These facts indicate that the reachable set function \(R_i(q_i(t))\) is a hyperrectangle:

**Theorem 1.** The reachable set function \(R_i(q_i(t))\) of the \(i\)-th robot is:

\[
\begin{align*}
R_i(q_i(t)) &= \\{x, y\} : \{x, y\} - (A_{i,x})^{K_i} q_{i,x}(t) \in RP_{i,x}(0) \times \{0\} \times \{0\}\}
\end{align*}
\]

Let us see if the reachable set function satisfies the two requirements. Since the reachable set function \(R_i(q_i(t))\) can be obtained by simply substituting \(q_i(t)\) value, Requirement 1 is achieved. Note that all the intermediate variables are hidden in the \(R_i(q_i(t))\), thus Requirement 2 is also satisfied.

### 5 Algorithm Analysis

In this section, we discuss the two important properties of the algorithm: feasibility and stability. We also compare the complexity of the proposed method with CMPMC on switched linear systems.

As the goal states given by the central controller at each collaboration cycle of all the robots can be exactly reached, the feasibility of HMPMC is determined by the optimal problem treated by the central controller. The central controller is aware of the status of all the robots and solves the optimization problem constrained by the complete collision avoidance specification, so the feasibility is automatically assured by the solution.
Theorem 2 (Feasibility). Our HMPC scheme is feasible.

The terminal constraint set and cost function methods are widely used to ensure the stability of traditional MPC approaches [Mayne et al., 2000]. They differ from each other on the setting of stable parameters (namely, a terminal cost $l_H$, a terminal constraint set $Q_f$ and a controller function $\kappa(\cdot)$). Since CMPC deals with the multi-robot system as a whole, these various approaches can be easily applied on CMPC. So instead of giving the concrete parameter setting, we show thefeasibility that the $H$MPC and CMPC are mixed integer programming (MIP). There is no available theory of MIP complexity analysis, we analyze their complexity by comparing the number of (scalar) variables and (scalar) constraints instead. As integer variables have great impact on the MIP complexity, we consider continuous and integer variables separately.

Proposition 1 (Complexity). Comparing to the optimization problem in CMPC, the one in our HMPC’s central controller is reduced by $H \cdot \sum_{i=1}^{N} (2K_i M_i x M_i y + 4K_i - 4)$ continuous variables, $H \cdot \sum_{i=1}^{N} K_i M_i x M_i y$ integer variables and $H \cdot \sum_{i=1}^{N} (2K_i M_i x M_i y + 4K_i - 3)$ constraints.

Proof. Collaboration specification and collision avoidance specification are treated the same in both control frameworks, thus we do not take them into account. For a robot $i$, at each sampling instant, there are $M_i x, M_i y$ integer switching control variables, $2M_i x, M_i y$ continuous control variables, $4$ continuous state variables, $2M_i x, M_i y + 1$ control constraints and $4$ state equation constraints, which should be all considered in CMPC. The intermediate variables and constraints in a collaboration cycle are reduced in our HMPC with the additional $4$ reachable set constraints. Since the optimization problems in our HMPC and CMPC’s central controller consider $N$ robots in $H$ collaboration cycles, the proposition is true.

Proposition 1 theoretically shows that our HMPC greatly reduce the number of variables and constraints comparing to CMPC. In the next section, the experiments results empirically support this conclusion.

6 Experimental Results

In order to explore the practicability of our HMPC based method on switched linear multi-robot systems, we have implemented other MPC schemes: centralized MPC (CMPC), basic DMPC (BDMPC), sequential DMPC (SDMPC), and iterative DMPC (IDMPC). CMPC [Dunbar and Murray, 2002] deploys a central controller to compute the concrete inputs of all the robots. On the contrary, DMPCs distribute the computation to many robots and differ from each other in terms of the policy of distribution: robots compute concurrently in BDMPC [Keviczky et al., 2004], sequentially in SDMPC [Kuwata and How, 2011], and iteratively in IDMPC [Mercangöz and Doyle III, 2007].

We derive the dynamic model of the $i$-th robot (Eq. 3) by discretizing a switched linear continuous system:

$$\dot{q}(t) = A q(t) + B_{r,s} u(t), t \geq 0, r, s \in \{1, 2\},$$

where

$$A = \begin{bmatrix} 0 & 0 & 1 \end{bmatrix}, \quad B_{r,s} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix},$$
at the sampling frequency:

\[
\text{sampling frequency of } i\text{-th robot} = \begin{cases} 
1/0.075, & i \mod 3 \equiv 1, \\
1/0.1, & i \mod 3 \equiv 2, \\
1/0.15, & i \mod 3 \equiv 0.
\end{cases}
\]

The continuous control constraint is \(U_i = [2, 2]^T\) and the safety distance is \(d_{oa} = 0.6\).

Programming problems embedded in MPCs are solved by the CVX, a Matlab-based package [CVX Research, 2012; Grant and Boyd, 2008].

### 6.1 Effectiveness

We compare the effectiveness by simulating MPCs with different numbers of robots \(N = 3, 6, 9, 12, 15, 18, 21, 24\). Our HMPC finishes all the simulations as CMPC. Due to the space limitation, we show the trajectories computed by our HMPC in 6-robot, 12-robot, 24-robot cases as Figure 1. In Figure 1 (and Figure 2), the \(x\)-axis and \(y\)-axis construct the plane which all the robots move in, and represent the positions of robots. Blue stars denote the initial positions, black crosses denote the goal positions, and dots in different colors denote the trajectories of different robots. In this configuration, robots have to cross the trajectories of others before they reach their goal positions. If all robots move directly towards the corresponding goal positions from initial positions, collision will inevitably happen.

Observing the trajectories computed by our HMPC, the robots in each scenario do not collide (satisfying feasibility) and finally converge to the goal states (satisfying stability), which conforms to the theoretical conclusion in Sec. 5.

However, DMPCs suffer from heavy failure issues, where several typical failed scenarios are shown in Figure 2. The reasons leading to failures fall into three main categories:

- **Incorrect Prediction**: In Figure 2a, the 3rd and 5th robots collide, even though they are neighbors. Instead of knowing the actual behaviors of its neighbors, in BDMPC each robot computes its action by prediction. These neighbors often behave differently from what the \(i\)-th robot predicts. As a result, it is of high possibility that two adjacent robots make incorrect predictions on each other’s behavior and thus collide.

- **Divergent Iteration**: In Figure 2b, the robots get stuck in an infinite loop as the iteration process does not converge when using IDMPC. Before it was forcibly terminated, the iteration had tried over 100 times and spent more than four hours. It indicates that IDMPC may need additional treatment when encountering navigation problems with non-convex constraints.

- **Aggressive Action**: In Figure 2c, the 10th robot cannot get a feasible solution. In SDMPC, robots compute their actions sequentially in a fixed order. The aggressive actions taken by the robots with high priority may push the robots with low priority out of feasible regions.

### 6.2 Efficiency

Figure 3a shows the computation time of different MPCs in the scenarios in Sec. 6.1. For each scenario, the average computation time at each collaboration instant is plotted, if a MPC scheme succeeds. We study the efficiency improvement accompanying the increment of robots. Notably, compared to CMPC, our HMPC improves the efficiency by at least 66.4% for all cases. This result complies with the theoretical conclusion in Sec. 5. The great reduction of constraints and variables makes our HMPC much more efficient in practice.

We then explore the efficiency improvement when the number of dynamic modes grows up. Figure 3b shows the result. The \(y\)-axis reflects the increasing rate of the average computation time at each collaboration instant, which is calculated by dividing the extra computation time in the case of four-mode robots by the computation time in the case of one-mode robots. The \(x\)-axis shows the number of robots involved. The average increasing rate of our HMPC is 61.8%, while that of CMPC is over 300%. It indicates that our HMPC is less sensitive to the growth of systems’ complexity than CMPC. It is due to the fact that in our HMPC the hyper-rectangle representation of reachable set hides the integer variables in the central controller introduced by multiple modes. Thus the complexity of the optimization problem in the central controller increases smoothly with the robot dynamic modes.

### 7 Conclusion

In this paper, we propose a novel HMPC based approach for the navigation problem of switched linear dynamical robots with a new reachable set computation technique. We discuss feasibility, stability and complexity of the approach theoretically and shows the effectiveness and efficiency empirically.
References


